

“Role of Alternative Aviation Fuels on Reducing the Carbon Footprint”

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الصندوق القطري لرعاية البحث العلمي

Qatar National Research Fund

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Micro Scale Thermo-Fluids Lab (MSTF), Texas A&M University at Qatar (TAMUQ)

- Role of alternative aviation fuels
- Introduction
- Collaborative research
- Fuels
- Research at MSTF-TAMUQ
- Takeaways
- Future directions

➤ Need for alternative fuels?

- ❖ Diversification / supply security
- ❖ Reduce environmental impact

➤ Alternative fuels sources?

- ❖ F-T based synthetic fuels (XTL)
 - X- Coal, Gas, Bio
- ❖ Hydroprocessed Renewable Jet Fuel (HRJ) / Hydroprocessed-Ester / Fatty acids (HEFA) – from vegetable oils / animal fats
 - Camelina, Jatropha, Algae, Tallow, used cooking oil etc.,
- ❖ Direct-Sugar-to-Hydrocarbon
- ❖ Alcohols-to-Jet (ATJ)

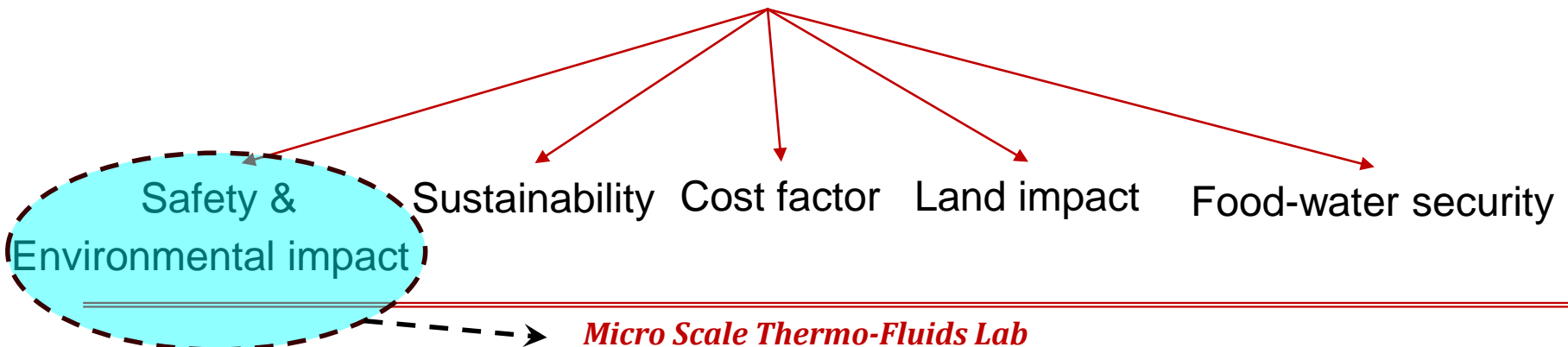
Aviation Alternative Fuels

➤ Developments / Milestones?



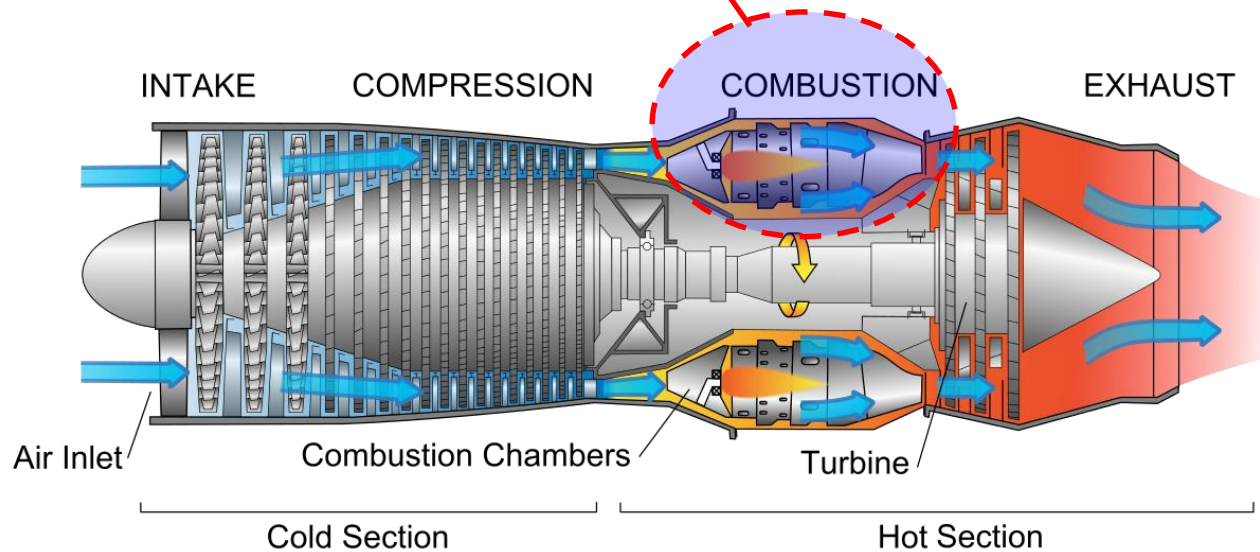
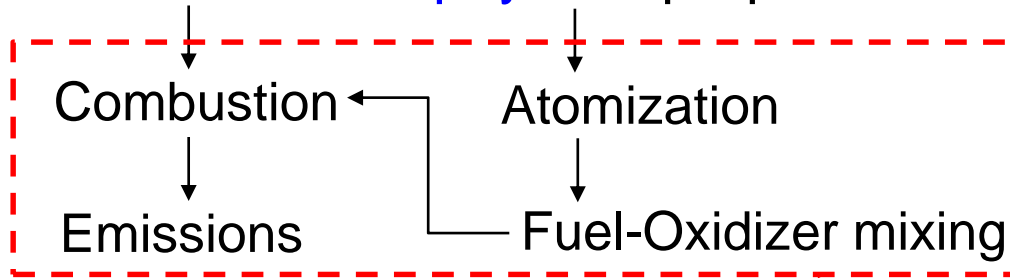
“A total of 21 airlines have now used alternative fuel for commercial flight. This is extremely impressive when just 5 or 6 years ago the entire concept was labeled as hypothetical.” - IATA report on Alternative Fuels, 9th Ed., Dec' 2014

Key challenges in developments?



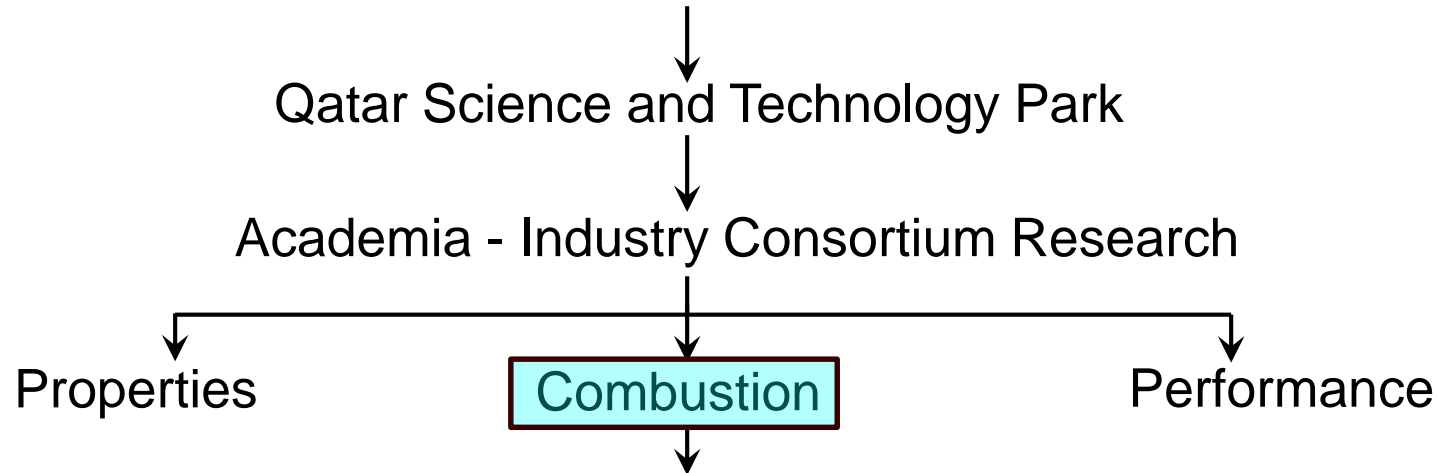
Safety / Environment?

- New fuel has to meet the performance standards of ASTM
- **Chemical** and **physical** properties – different



source: Internet

- Abundance of Natural gas in Qatar instigated interest in “Gas-to-Liquid (GTL)” fuel as *drop-in* fuel for aviation engines



- *Part-1 : High altitude relight ignition tests at R-R, UK*
- *Part-2 : Emission tests at R-R, USA*
- *Part-3 : Combustion studies at DLR, Germany*
- **Part-4 : Atomization study at TAMUQ, Qatar**

GTL Fuels : Shell

Gas-To-Liquid (GTL) : liquid fuel synthesized from Natural gas using Fischer-Tropsch

➤ Effect of fuel composition on combustion;

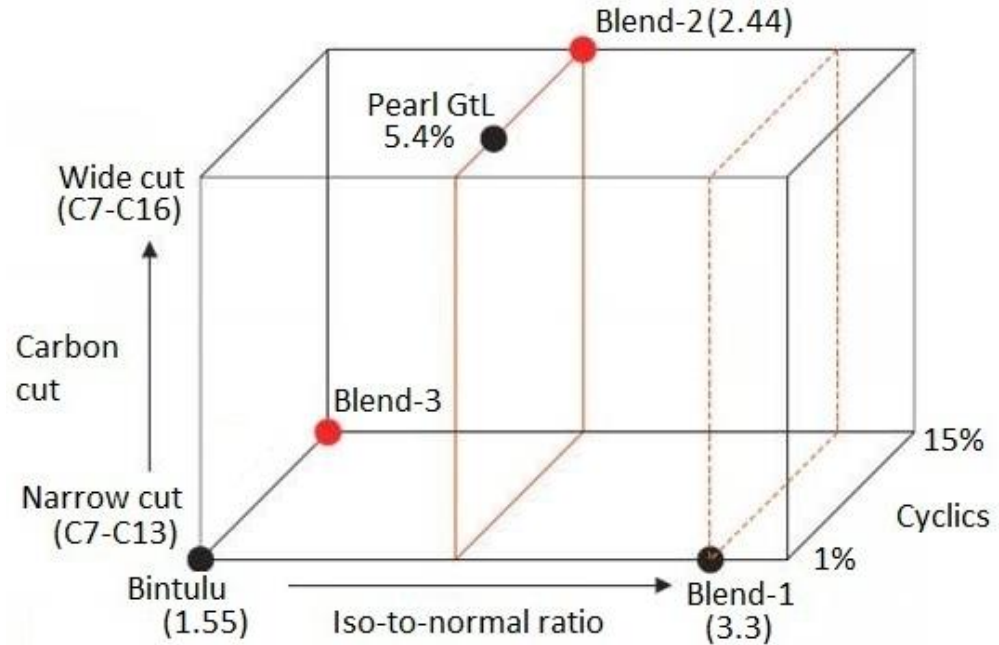
- ❖ Carbon range
- ❖ Iso-to-normal paraffin ratio
- ❖ Cyclic content

➤ Five GTL fuels – Shell

- ❖ **Two** commercial fuels
 - ❑ Bintulu GTL - Malaysia
 - ❑ Pearl GTL - Qatar

- ❖ **Three** blends:
(Bintulu + “ShellSol”)

➤ Reference fuel: Conventional “Jet A-1”



[Bauldreay et al., 2011]

Fuel properties: Shell

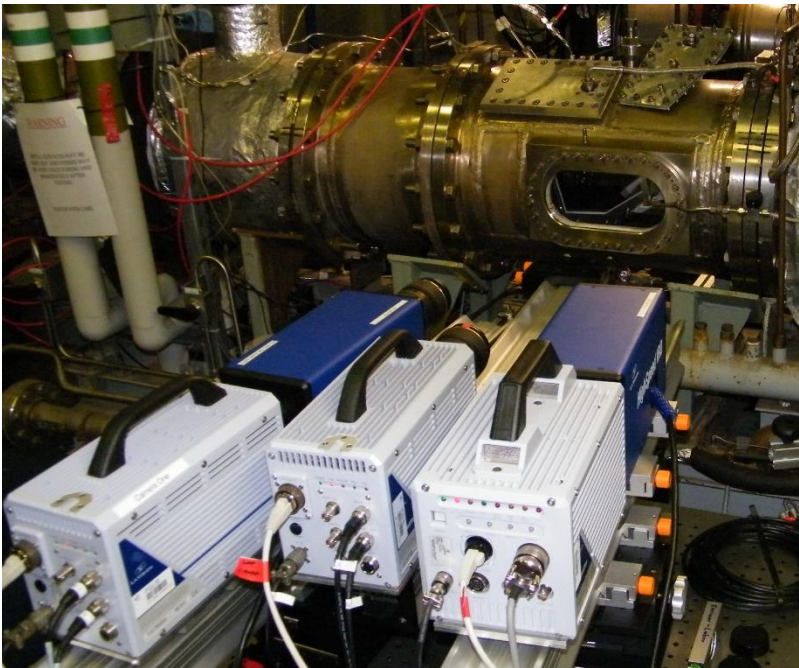
Properties @ 20°C	Blend-1	Bintulu (CSPK 1)	Blend-3	Blend-2	Pearl (CSPK 2)	Jet A-1
Density (kg/m ³)	746	738	751	763	749	790
Viscosity (mm ² /s)	1.36	1.37	1.46	1.60	1.55	1.68
Surface tension (mN/m)	23.8	23.5	24.1	24.2	23.9	26.8
H/C ratio (measured)	2.2	2.3	2.2	2.2	2.2	1.92
Iso-paraffins (% Wt)	73.3	55.7	48.4	58.1	64.8	NA
Normal paraffins (% Wt)	26.0	43.4	36.5	26.7	29.8	NA
Iso-to-normal paraffin ratio	3.3	1.6	1.5	2.4	2.5	NA
Naphthenes (% Wt)	0.4	0.5	15.4	15.6	5.4	NA
Carbon Cut Narrow (C7-C13) / Wide (C7-C16)	Narrow	Narrow	Narrow	Wide	Wide	NA
Distillation Characteristics (°C)						
T50 - T10	8.4	16.6	8.4	10	9.4	28.5
T90 - T10	20.7	22.5	21.2	27.5	28.7	68.3

➤ Calorific value (LHV as per D4809 standard) : 43.3 ~ 44.2 MJ/kg

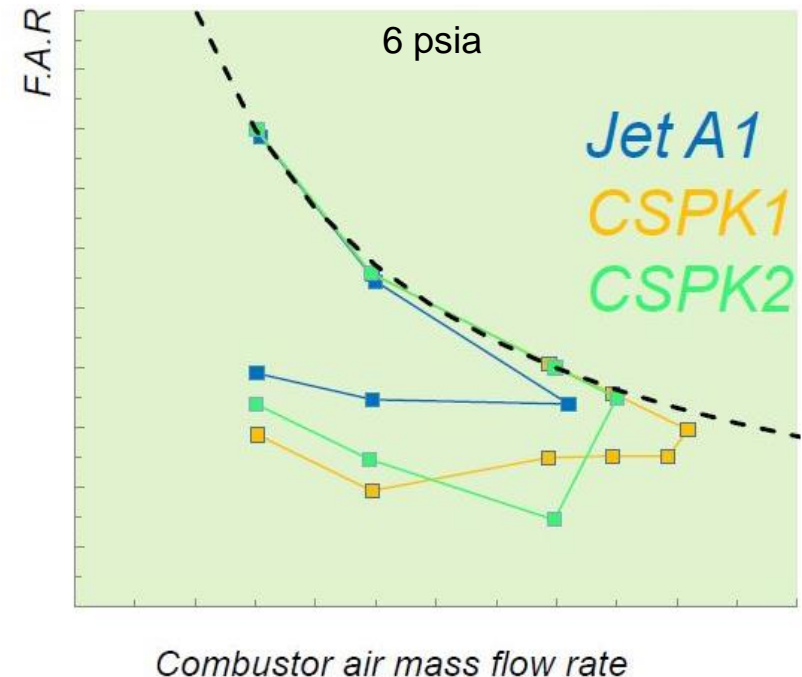
Part-1: Relight Ignition

(RR-UK, DLR-Germany, TAMUQ-Qatar)

- High altitude relight ignition tests
- Sub-atmospheric combustion rig – Rolls-Royce, Derby-UK
- Limits of ignition boundary tested at two combustion inlet air pressures



(Rolls-Royce-UK facility equipped with DLR diagnostics)



Proceedings of ASME Turbo Expo 2011: Power for Land, Sea and Air, June 6-10, 2011, Vancouver, Canada:

- Darren et al., (2011), GT2011-45487
- Thomas et al., (2011), GT2011-45510

Part-2: Emission Tests

(RR-UK, RR-US, TAMUQ-Qatar)

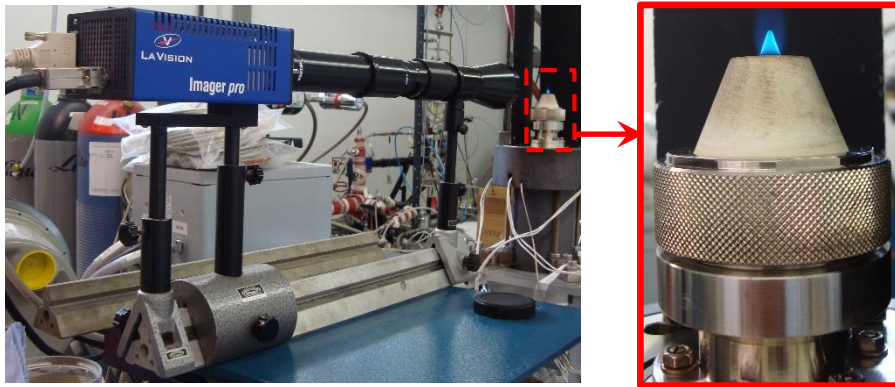
- Emission characteristics : NO_x , CO, CO_2 , UHC, and smoke number
- IP - Combustion chamber facility at RR-Indianapolis, USA
- Test conditions - represent different stages of aircraft engine cycle – ICAO standards
- Both Main & pilot-scale nozzles were used in emission tests

Emission Tests Outcome:

- At a given combustor operating condition, GTL produced **less smoke** than Jet A-1
- Under some cases, GTL produced **more NO_x** than Jet A-1 fuel
- Further studies are necessary to gain more insights

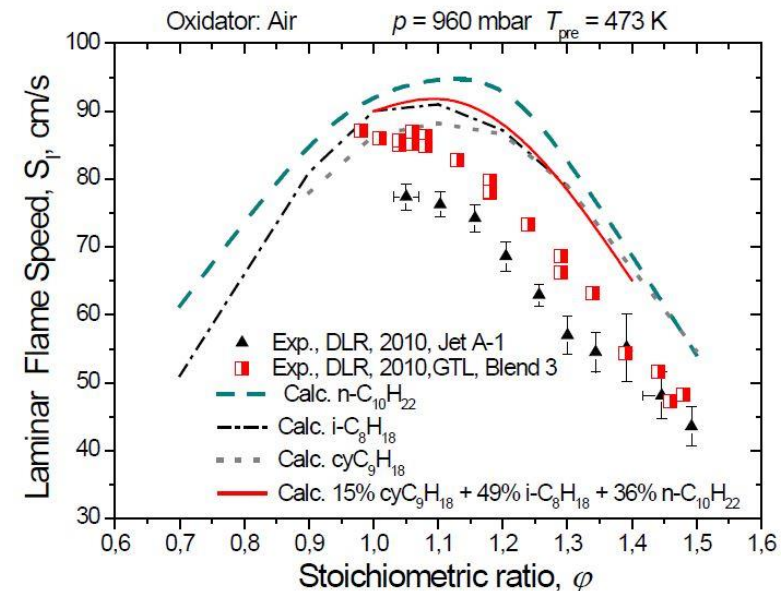
(DLR-Germany, TAMUQ-Qatar)

- Laminar flame speed measurements at atmospheric conditions



(Atmospheric-Laminar flame speed facility, DLR)

- Ignition delay measurements: Shock tube
- Surrogate chemical kinetics – GTL fuel



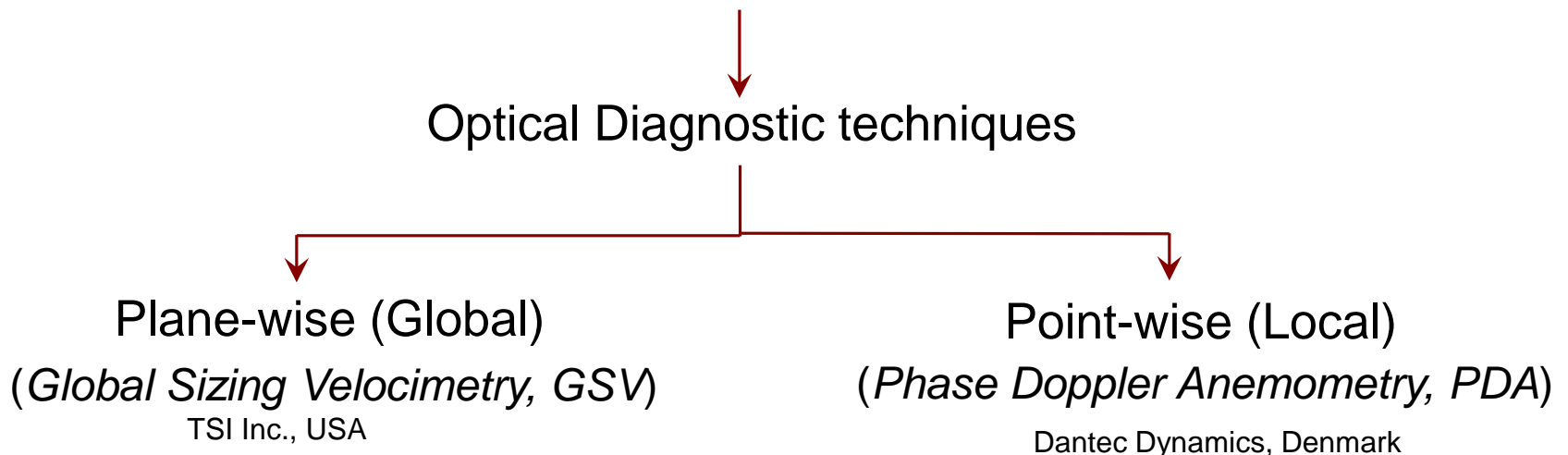
- Kick et al., Energy 43 (1), 111-123, 2012

- Slavinskaya et al., "Surrogate Model Design for GTL Kerosene", *50th AIAA Aerospace Sciences Meeting and Exhibit*, Tennessee, USA, 9-12 Jan, AIAA-2012-0977.

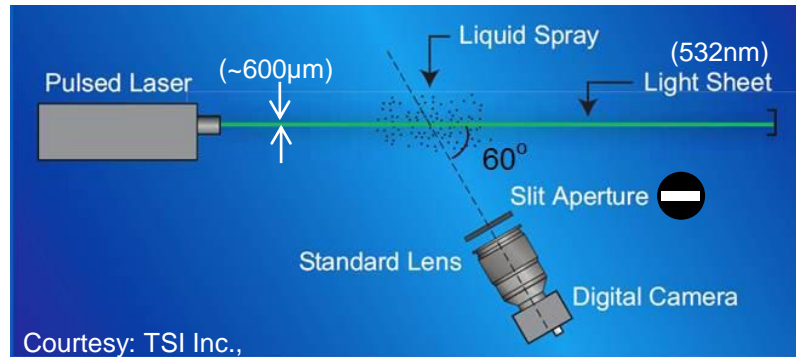
Need for spray characteristics?

- Change in physical properties, viscosity, density and surface tension affects the fuel “atomization” characteristics
- Atomization → fuel-air mixture → **Combustion** → **Emissions**

“*Microscopic*” spray characteristics: Droplet size and velocity distribution
(GTL vs Jet A-1)



GSV Technique



- Fringe spacing is most “*insensitive*” to refractive index at 60° (Pan et al. 2005)
- Light scattered by the droplets exhibit angular oscillations (fringes)
- Droplet size is proportional to the fringe spacing (Pan et al. 2005)

Droplet size measurement limits*

$$27\mu\text{m} < d < 2\text{mm}$$

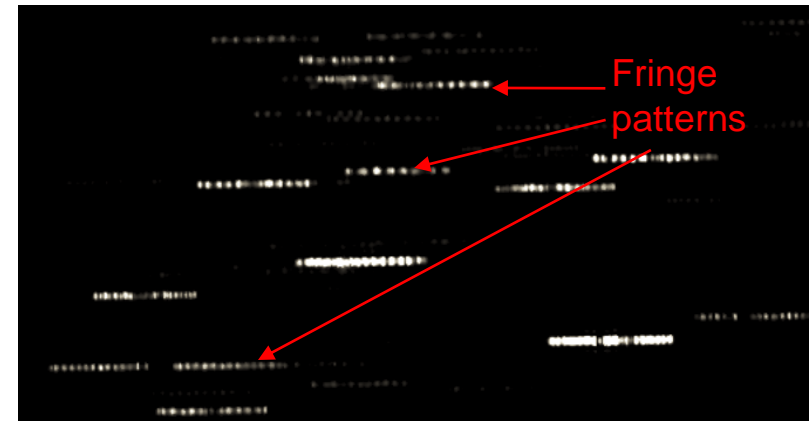
* Limits vary with,

- camera resolution, defocus distance, Magnification, Aperture size

Lorenz-Mie scattering theory

Out-of-focus image (Ragucci et al. 1990)

Flow ↓ direction

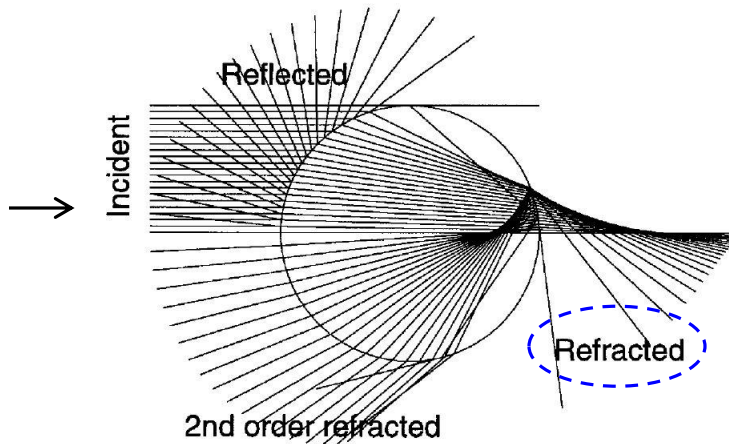


Imaging details

- 200 image pairs (2Hz frame rate)
- 1600x1200/ binning (2x2)
- defocus distance: 135 mm
- Aperture number: 4

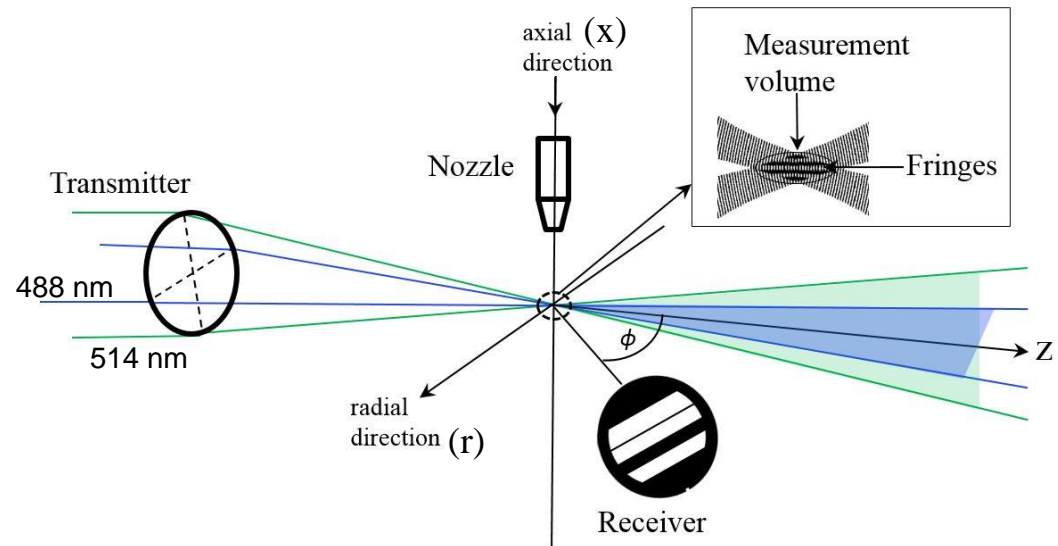
PDA Technique

- 2-D PDA system
- $\lambda = 514\text{nm}$ (axial) and 488nm (radial)
- Diameter – Doppler burst phase shift
- Velocity – Doppler burst frequency



Courtesy: Dantec Dynamics

Lorenz-Mie scattering theory



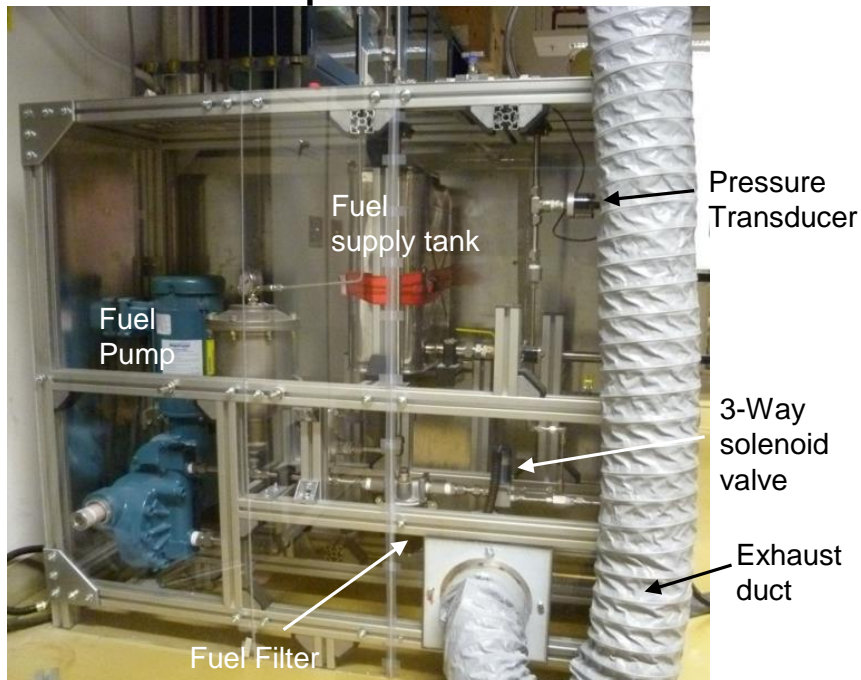
Transmitter and receiver probe arrangement

- Receiver probe is positioned at 42° (ϕ)
- Data sampling: 10,000 samples or 15s
- Results presented are an average of three best trials
- Validation: Diameter (60-80%)
Velocity (80-90%)

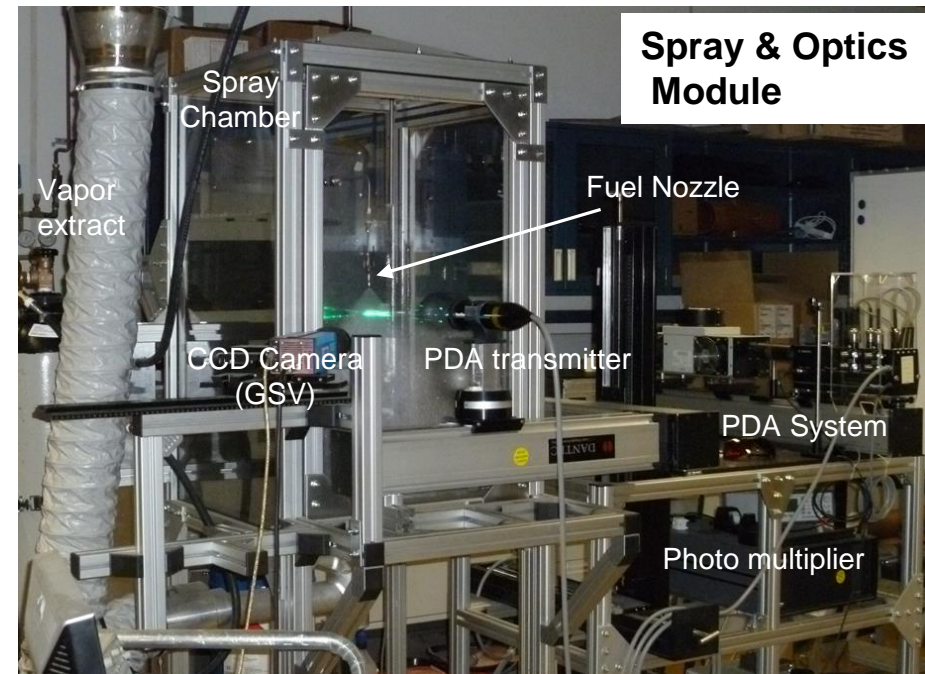
Experimental Facility

- Three modules – Pump, Spray and Optics
- High pressure fuel supply loop
- Nozzle supplied by RR-UK is mounted on a traversing system
- Injection pressure is measured just upstream of the nozzle
- GSV & PDA systems are integrated to the facility

Pump Module

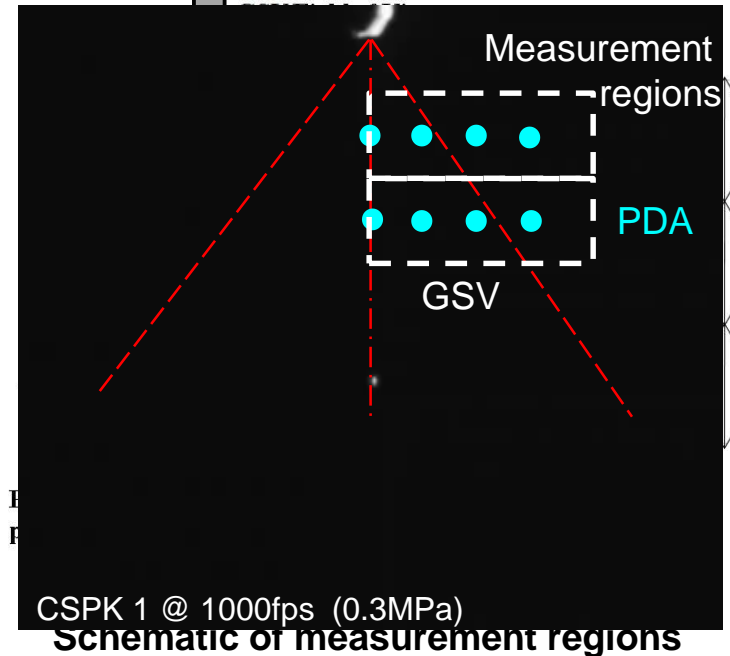


Spray & Optics Module

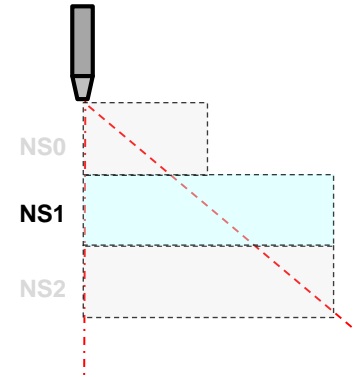
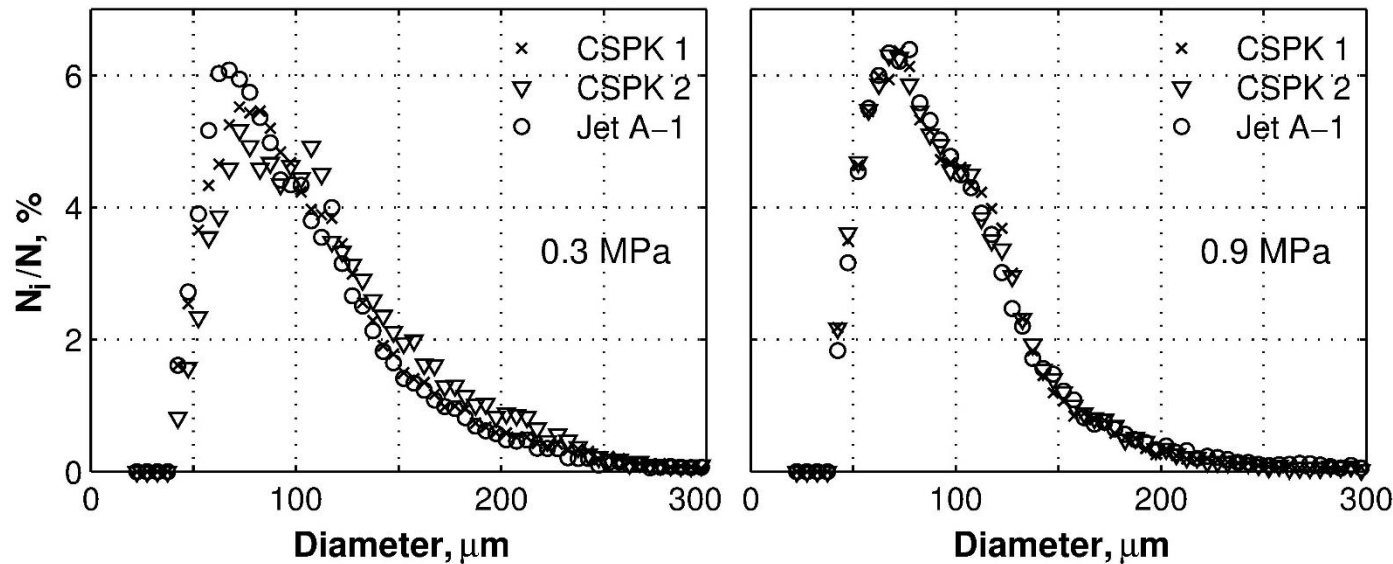


Experiment Details

- Inert (N_2) ambiance at atmospheric condition (101325Pa and 298K)
- Pilot-scale pressure-swirl nozzle: Fuel injection pressures are 0.3, 0.6, and 0.9 MPa (SD $\pm 3\%$)
- Injection pressures are chosen based on RR-UK suggestions
- Spray is symmetric and measurements are carried out only on one side of the spray
- The field of view for GSV is decided based on the facility dimensions, camera lens capability. Radial direction is covered in two steps



GSV: Size Distribution at NS1

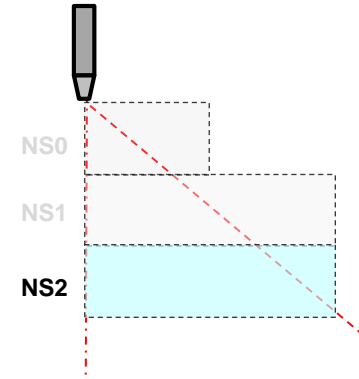
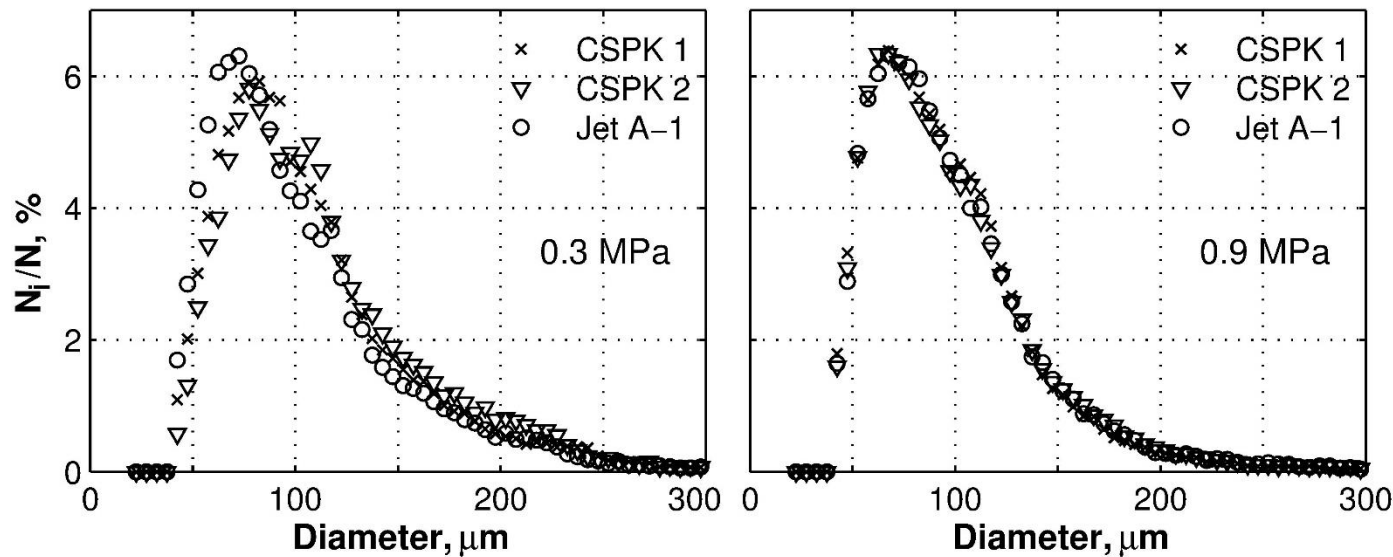


- The difference in size distribution beyond 300 μm is insignificant among the fuels and not shown
- However, full diameter range is used to calculate Sauter Mean Diameter (SMD)
- Increase in injection pressure slightly increases the number of smaller droplets as expected
- Distribution trends are similar

[Kumaran & Sadr, *ICLASS*, 2012]

[Kumaran & Sadr, *Atomization and Sprays*, 24 (7), 575-597, 2014]

GSV: Size Distribution at NS2

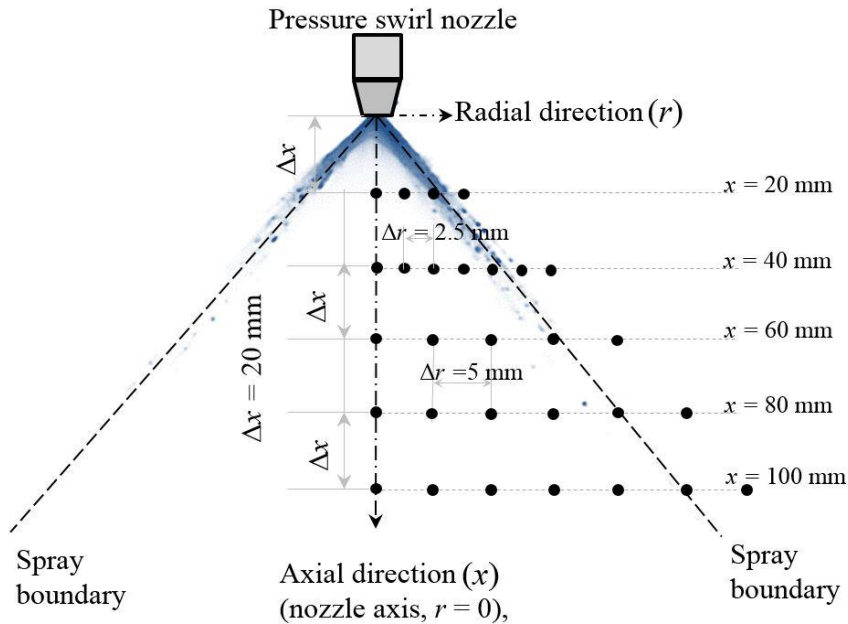


- Size distributions trends at NS2 are similar to that in NS1
- The probability is slightly higher at NS2 than NS1
- Mean droplet diameters (d_{10} and d_{32}) decrease with an increase in injection pressure as expected
- The mean diameter trends are consistent with those of the size distributions

[Kumaran & Sadr, *ICLASS*, 2012]

[Kumaran & Sadr, *Atomization and Sprays*, 24 (7), 575-597, 2014]

PDA Measurement Points



Operating Parameters

Transmitting optics

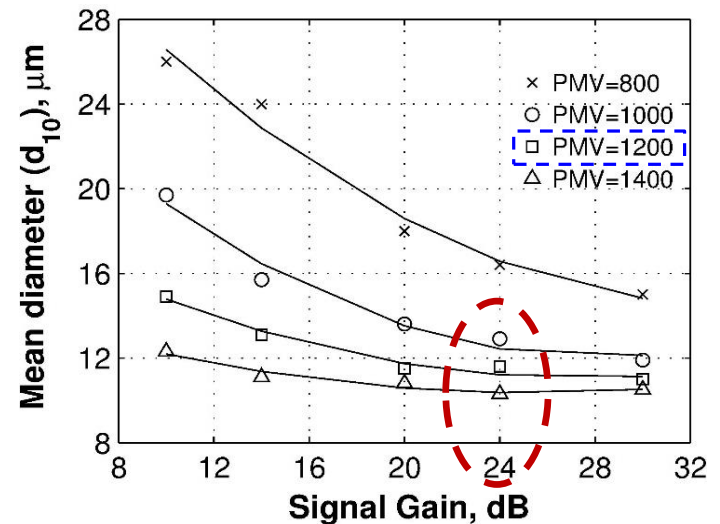
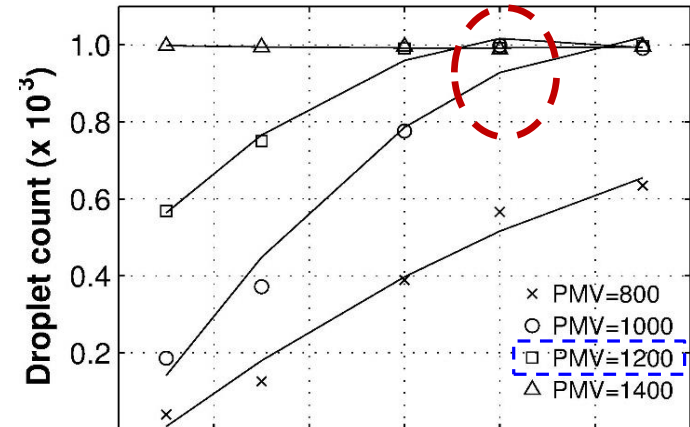
Focal length	400 mm
Beam spacing	38 mm
Beam waist	1.35 mm

Receiving optics

Focal length	500 mm
Scattering angle	42 °
Aperture mask	Mask-B

Measurement volume

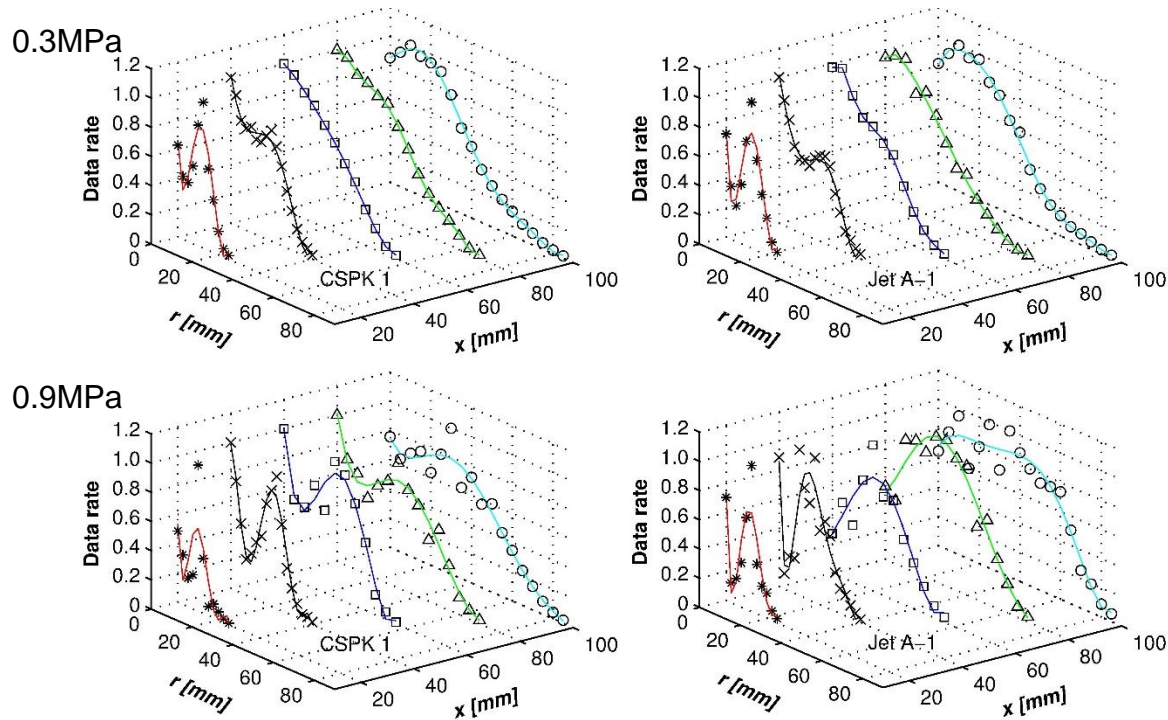
Diameter (dx)	189 μm
Length (dz)	3.97 mm
Fringe spacing	5.27 μm
No. of Fringes	36



User Settings

Photomultiplier Voltage (PMV)	1200 V
Signal Gain (SG)	24 dB
Signal-to-Noise ratio (SNR)	-2.0 dB

Normalized Data Rate

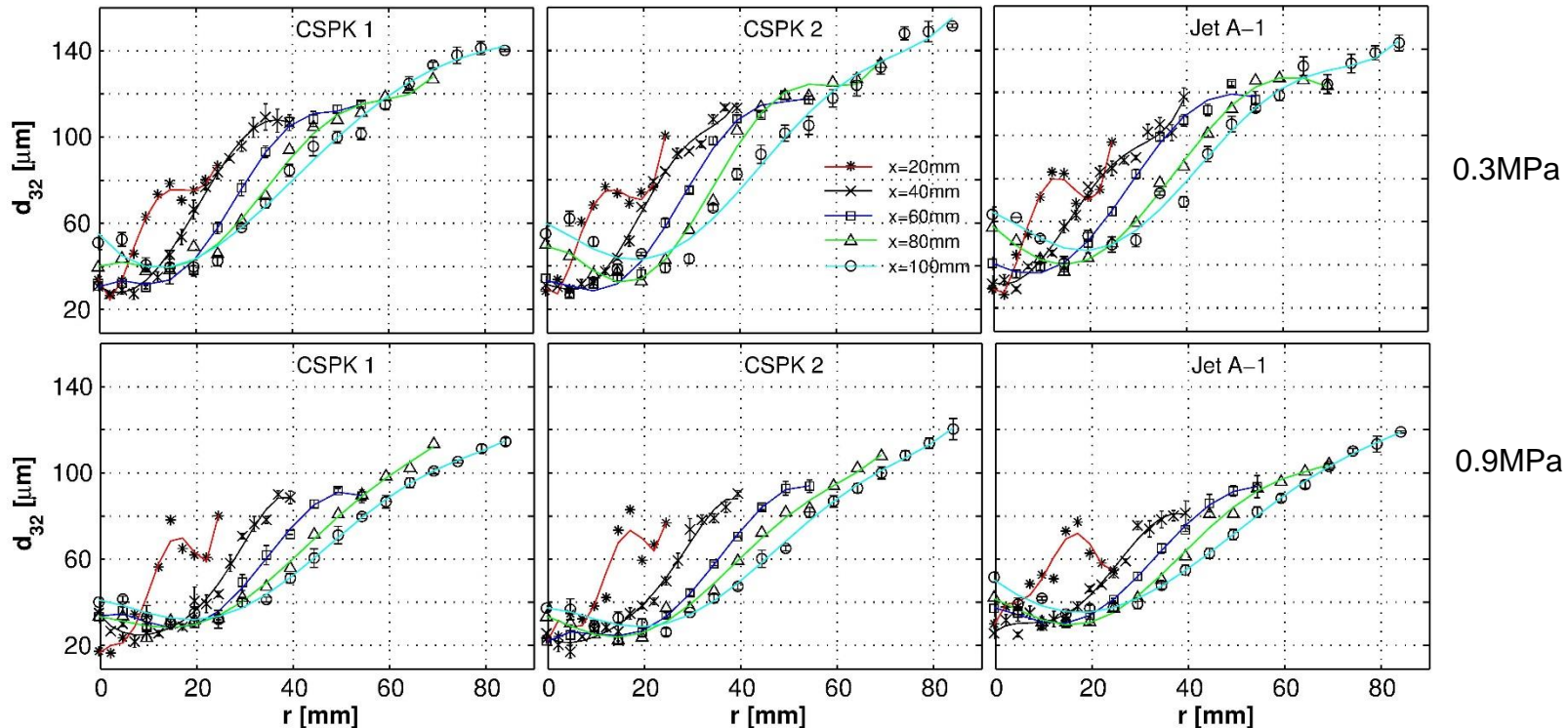


Only CSPK 1 & Jet A-1 are shown as they show maximum difference in their fuel properties

- Data rate at last measurement location is less than 3% of the maximum value at that axial location
- Lower values of viscosity and surface tension for CSPK 1: faster disintegration and dispersion of droplets when compared to that in Jet A-1 fuel

Sauter Mean Diameter (d_{32})

$$d_{32} = d^3 / d^2$$



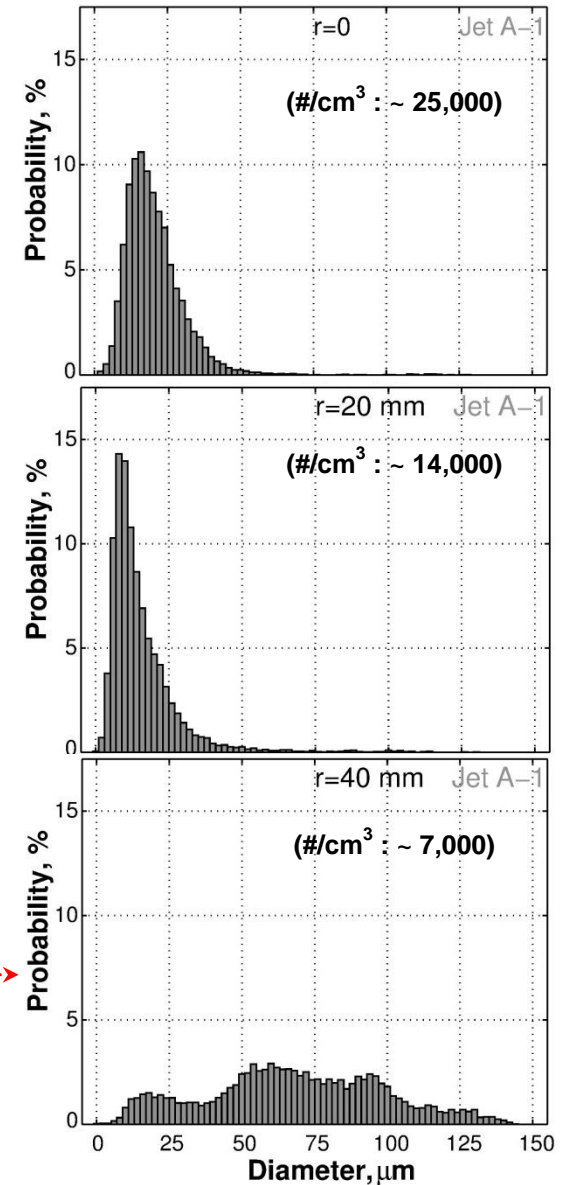
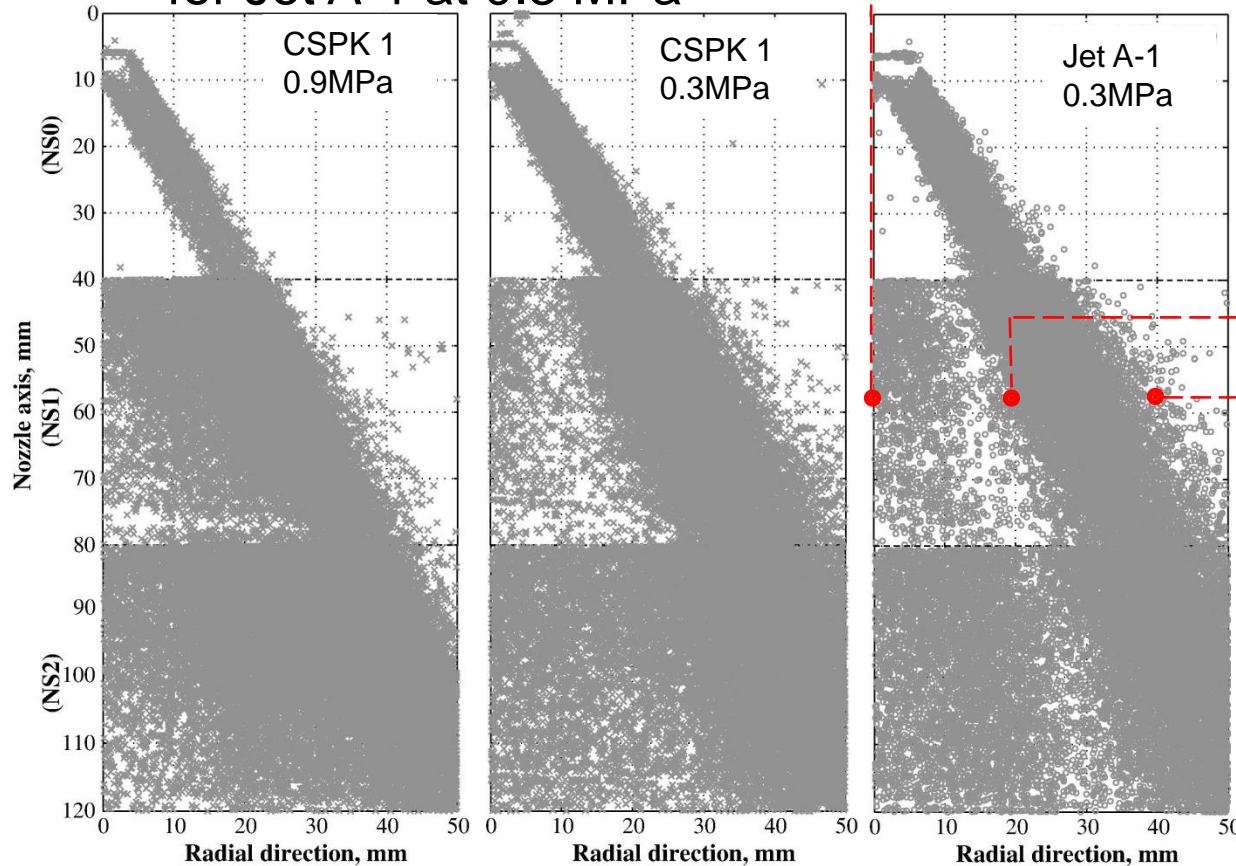
- SMD increases with increase in radial distance for all the fuels as expected in a pressure-swirl nozzle
- CSPK 2 and Jet A-1 trends are similar as their fuel properties are narrowly separated

[Kumaran & Sadr, *Ener.Conv.Mang.*, 88, 1060-1069, 2014]



Spatial distribution

- Spatial distribution of droplets detected using GSV
- “PDA measurements” at three radial locations for Jet A-1 at 0.3 MPa



GTL vs Jet A-1

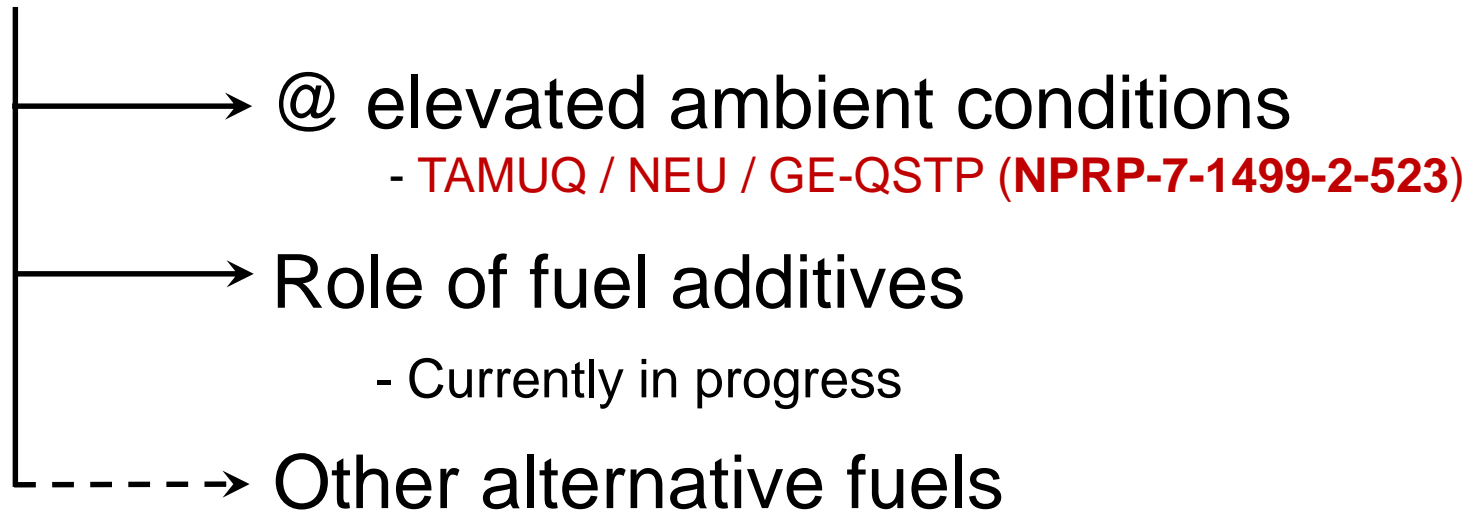
- ✓ Better ignition limits at high altitude conditions
- ✓ Better smoke performance

More NO_x emissions than Jet A-1

- ✓ Laminar flame speeds are slightly higher
- ✓ Overall spray characteristics are similar at atmospheric conditions

- Essential to study spray characteristics at actual combustor conditions

Spray Characteristics



↓
*Mixing / Combustion
aspects*

Only a drop in the ocean...



every drop counts! 😊

Acknowledgement

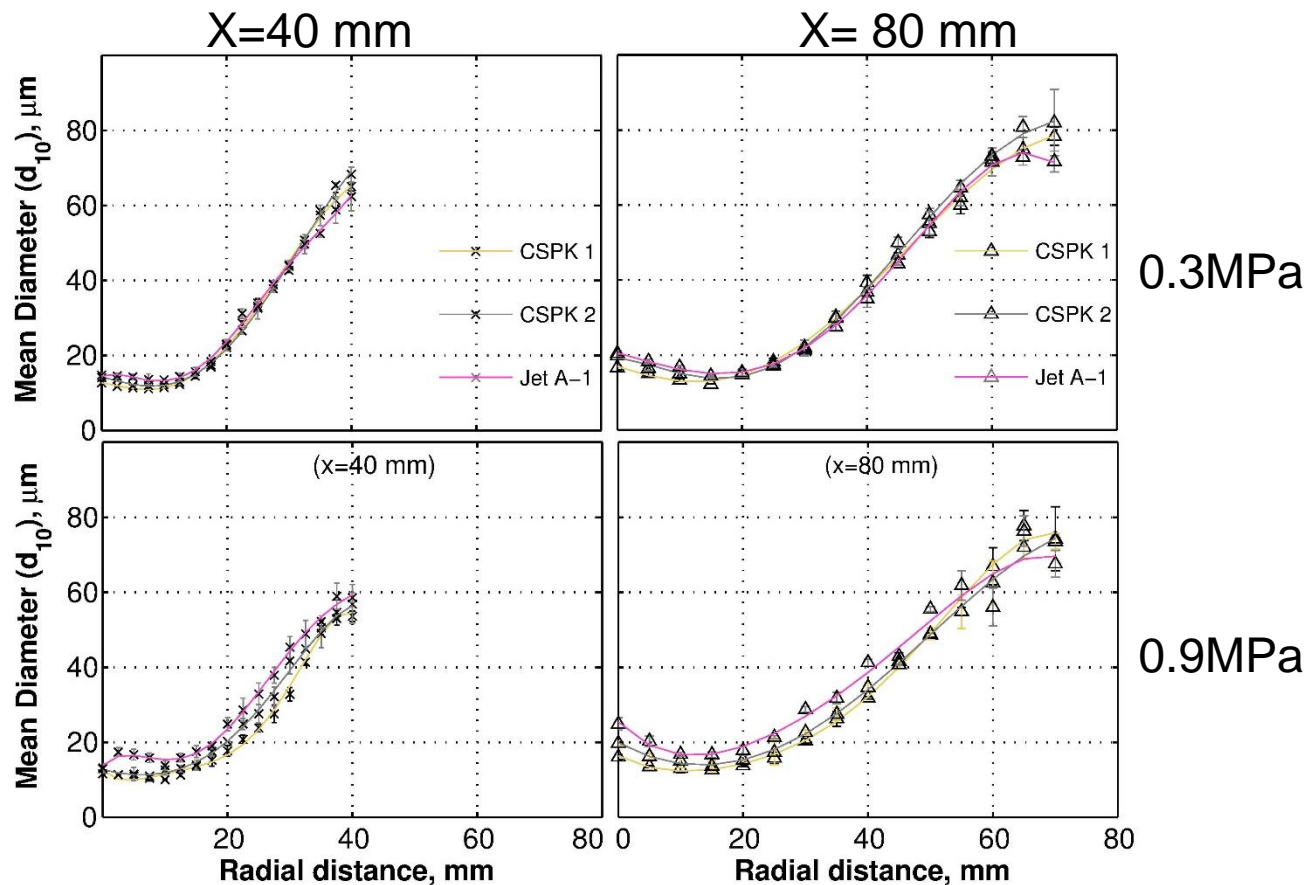
- **Rolls Royce, UK**
 - ❖ Mr. John Moran, Combustion Specialist
 - **DLR, Germany team**
 - ❖ Dr. Patrick LeClercq
 - ❖ Dr. Thomas Mosbach
 - **Shell (UK & Qatar) team**
 - ❖ Dr. Joanna Bauldreay, (UK)
 - ❖ Mr. Ali M. Al-Sharshani, (QSRTC)
- *late* Prof. Chris Wilson, University of Sheffield
- Dr. Mahesh Panchagnula, Indian Institute of Technology Madras (IITM)

Thank You!

- ❖ J. M. Bauldreay, P. F Bogers and A. Al-Sharshani, (2011) “Use of surrogate blends to explore combustion-composition links for synthetic paraffinic kerosines”, 12th International conference on stability, handling and use of liquid fuels, Florida, 16-20 October.
- ❖ Kumaran Kannaiyan and Reza Sadr, (2014) “Experimental investigation of spray characteristics of alternative aviation fuels”, ***Energy Conversion and Management***, 88, pp. 1060-1069.
- ❖ Kumaran Kannaiyan and Reza Sadr, (2014) “Effect of fuel properties on spray characteristics of alternative jet fuels using Global Sizing Velocimetry”, ***Atomization and Sprays***, 24 (7), pp. 575-597.
- ❖ Kumaran Kannaiyan and Reza Sadr, (2014) “Experimental study of the effect of fuel properties on Spray performance of alternative jet fuel”, ***Proceedings of ASME Turbo Expo 2014***, Vol. 3A, June 16-20, 2014, Dusseldorf, Germany, GT2014-25842.
- ❖ Kumaran Kannaiyan and Reza Sadr, (2013) “Spray Characteristics of Fischer-Tropsch Alternate Jet Fuels”, ***Proceedings of ASME Turbo Expo 2013: Power for Land, Sea and Air***, Vol.2, June 3-7, 2013, San Antonio, Texas, USA, GT2013-95761.
- ❖ Kumaran Kannaiyan and Reza Sadr, (2012) “Spray Characterization of Gas-to-Liquid Synthetic Aviation Fuels”, ***12th Triennial International conference on Liquid Atomization and Spray Systems (12th ICLASS)***, Heidelberg, Germany, September 2-6. (ISBN 978-88-903712-1-9)

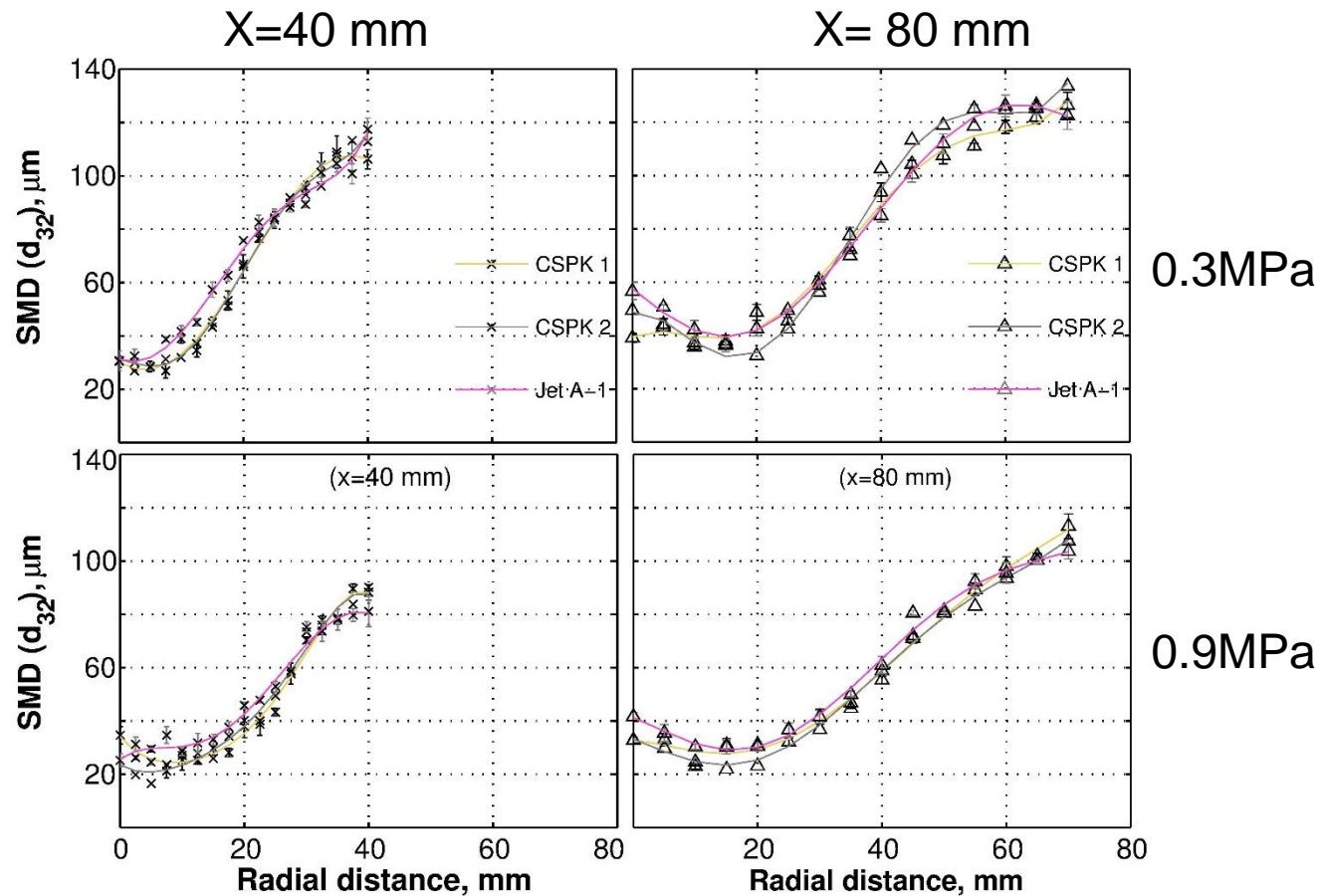
Mean Droplet Diameter (d_{10})

Compared across fuels at,



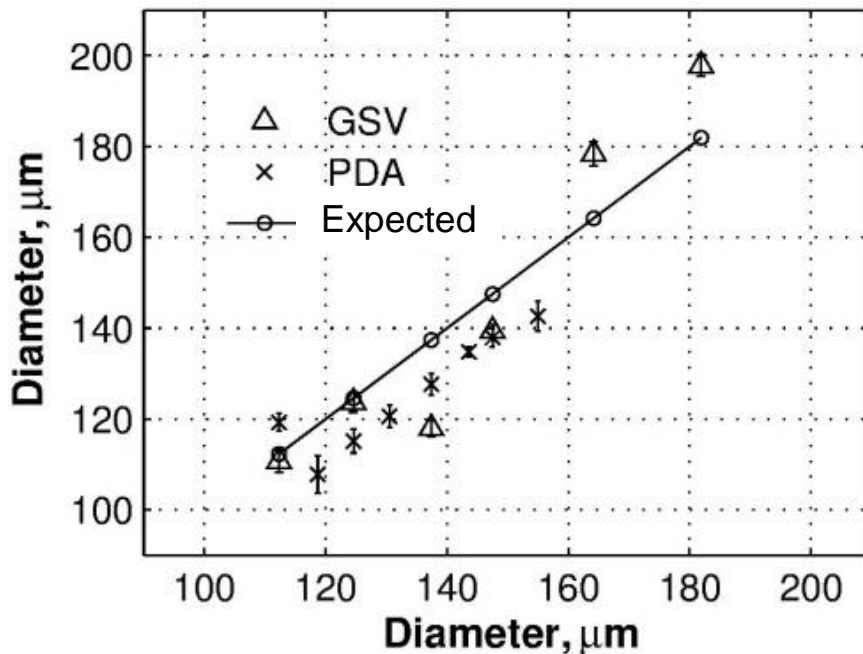
Sauter Mean Diameter (d_{32})

Compared across fuels at,

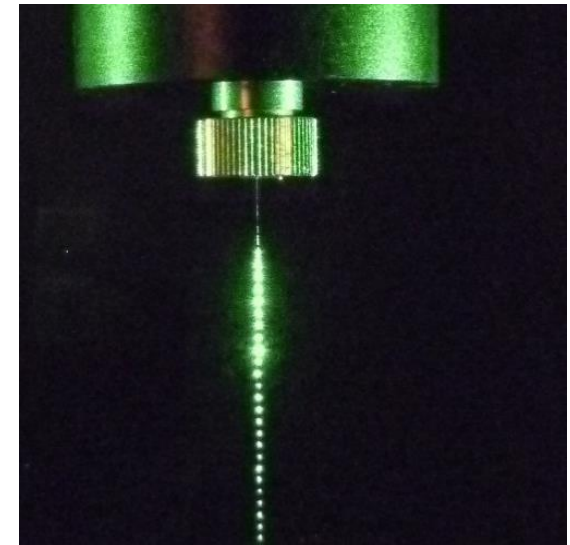
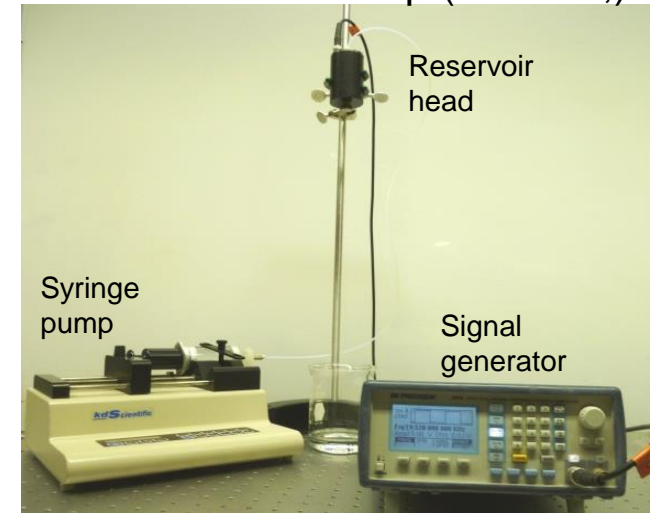


Verification

- Mono-disperse droplet generator (MDG) produces droplet diameters of known size
- Water is used to generate droplet diameters of known size
- GSV, PDA and expected diameters are within 10% agreement

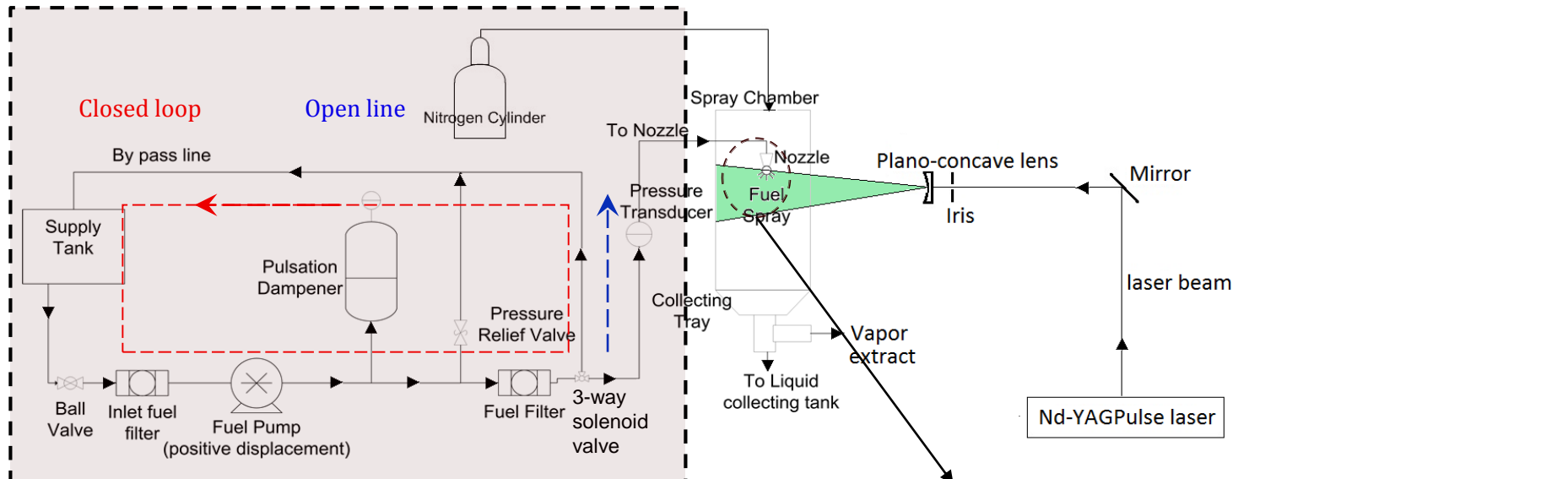


MDG-100 Setup (TSI Inc.,)

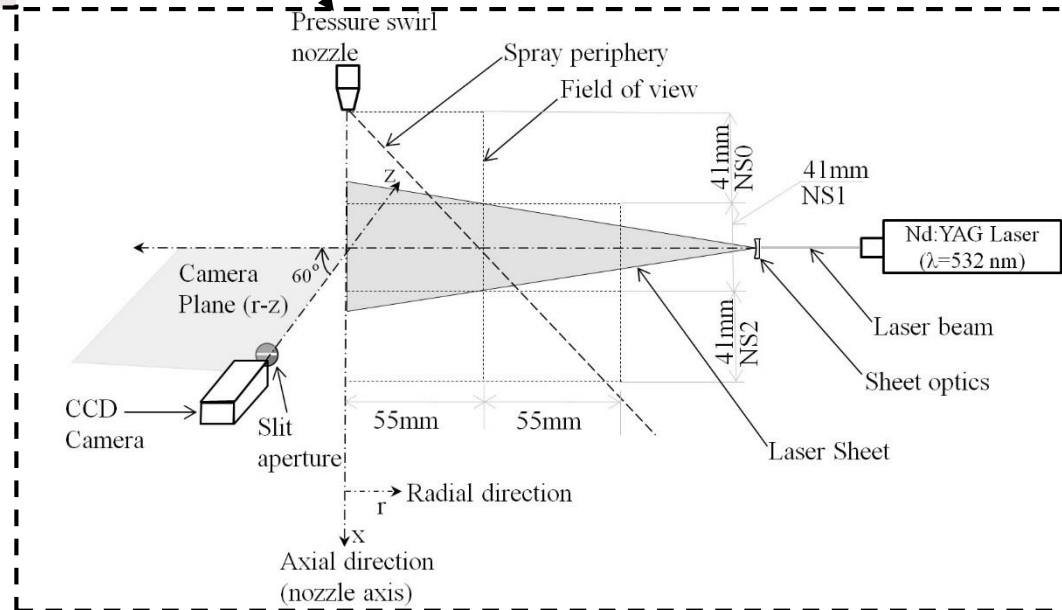


Water droplet stream from MDG

GSV Measurement Region



Fuel preparatory steps are the same for GSV & PDA measurements



SMD Comparison

- Estimated SMD using Lefebvre's (1987) empirical relation for Simplex nozzle,

$$SMD = 2.25 \cdot \sigma^{0.25} \cdot \mu_l^{0.25} \cdot \dot{m}_l^{0.25} \cdot \Delta P_l^{-0.5} \cdot \rho_a^{-0.25}$$

Injection pressure	SMD, μm (Estimate)		
	CSPK 1	CSPK 2	Jet A-1
0.3MPa	129	129	135
0.9MPa	93	95	98

GSV

- The SMD determined using GSV data is found to be higher than the estimated value by a maximum of 26% and 48% for 0.3MPa and 0.9MPa, respectively

Injection pressure	SMD, μm (GSV)		
	CSPK 1	CSPK 2	Jet A-1
0.3MPa	155	164	151
0.9MPa	136	138	145

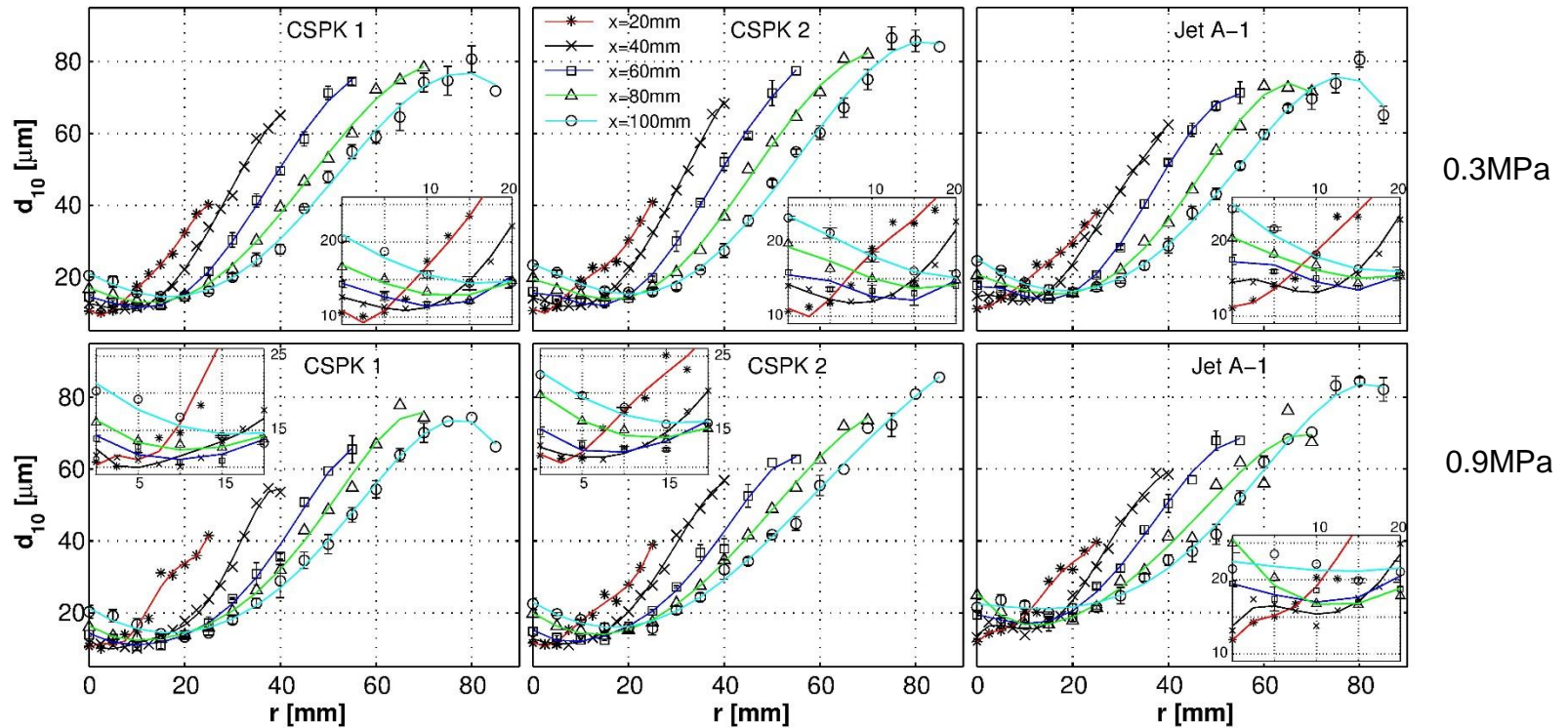
PDA

- Droplet diameters that are collected within a common time window across all radial locations at a given axial location are used for global SMD calculation.
- Global SMD is found to be lower than the estimated SMD by a maximum of 28% and 16% for 0.3MPa and 0.9MPa, respectively

Injection pressure	SMD, μm (PDA)		
	CSPK 1	CSPK 2	Jet A-1
0.3MPa	96	98	95
0.9MPa	81	83	82

[Kumaran & Sadr, ASME Turbo Expo 2013, GT2013-95761]

Mean Droplet Diameter (d_{10})

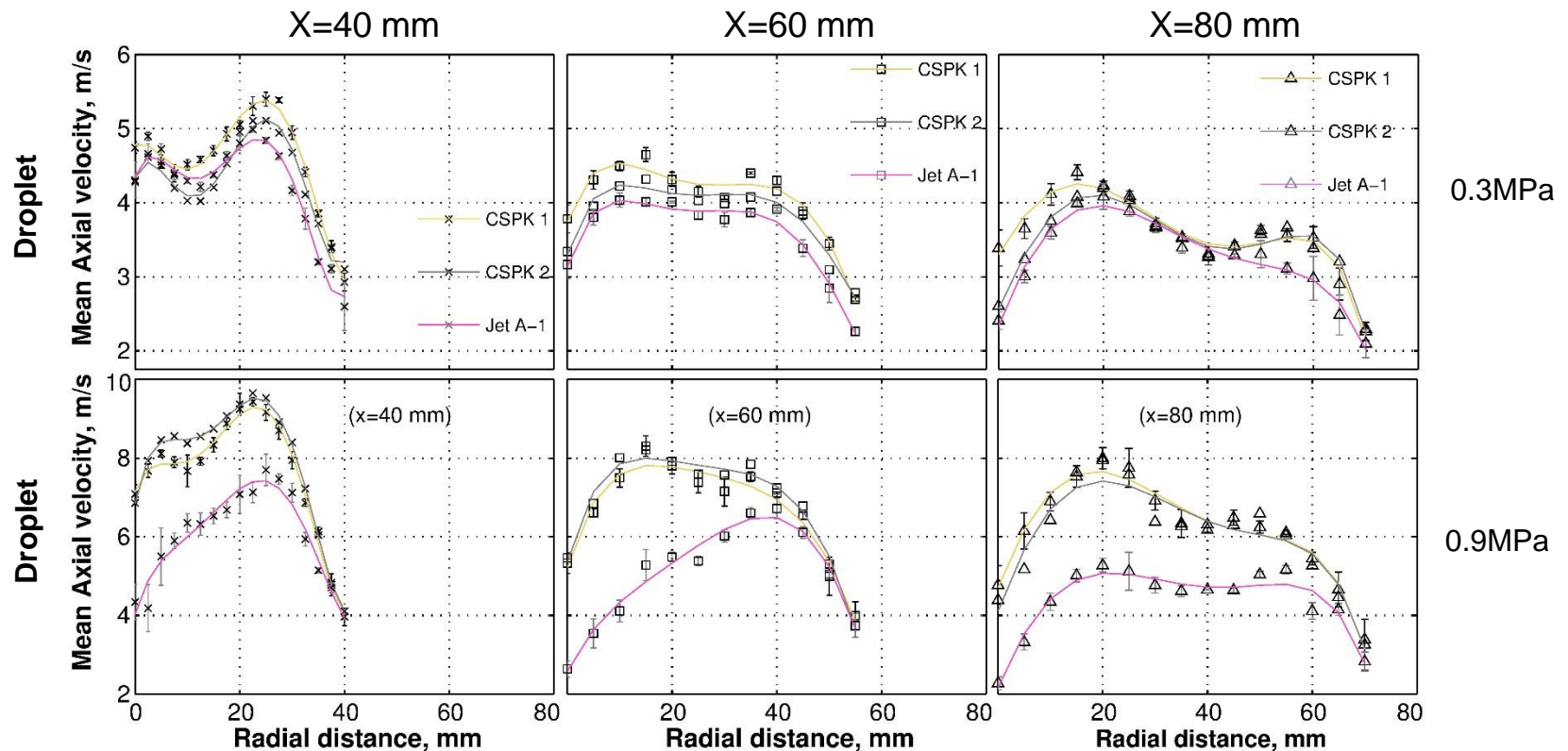


- Overall shape and trends are similar between the fuels.
- Typical standard deviation is shown as error bars only at two axial locations to facilitate the comparison

[Kumaran & Sadr, ASME Turbo Expo 2014, GT2014-25842]



Mean Droplet Velocity



- Fuel with lower viscosity and density (CSPK 1) exhibits higher droplet mean axial velocity
- Trends are inline with those observed for the data rate

[Kumaran & Sadr, *Ener.Conv.Mang.*, 88, 1060-1069, 2014]